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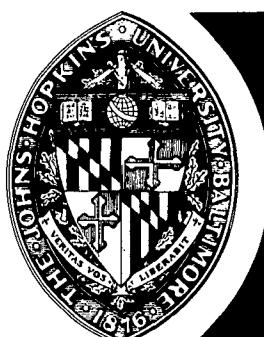
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Technical Report No. AF-105

**WAVE FUNCTIONS, ENERGIES, AND REDUCED MATRIX
ELEMENTS OF THE $5f^3$ CONFIGURATION
IN INTERMEDIATE COUPLING**

by

Hannah M. Crosswhite



**THE JOHNS HOPKINS UNIVERSITY
CARLYLE BARTON LABORATORY
BALTIMORE, MD.**

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ERRATA - AF 104 - A Forming Study of Point-Contact Tunnel
Diodes - H. J. Lory - May 1963

Page 11 line 9 reads aresnic - should be arsenic

Page 20 line 12 reads normal of N- should be - normal or N-

Page 35 equation (8) should be $\sqrt{2}$ $2\pi\epsilon e$ in the denominator

Page 88 line 14 reads H on D_o , should read H or D_o .

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ABSTRACT

Since the crystal field can be considered as a perturbation of the free ion spectra of actinide ions in certain crystals, we have calculated energy levels and wave functions of the $5f^3$ configuration, which is the ground configuration of U^{3+} , in intermediate coupling for values of $\chi = \zeta / F_2$ of 7 to 11. Energy levels are given in units of F_2 , and wave functions are expressed as linear combinations of Russell-Saunders functions. Hydrogenic and non-hydrogenic approximations are compared.

Reduced matrix elements in intermediate coupling are given so that crystal field splittings may be calculated. The splittings of the two lowest levels of U^{3+} in a weak field with and without J-mixing are compared.

I. INTRODUCTION

In the triply ionized actinides the optically active electrons belong to the $5f^n$ configuration^{1, 2}, so comparison of their spectra with those of the triply ionized rare earths, whose optically active electrons belong to the $4f^n$ configurations, is of considerable interest. The effect of the crystal field on rare earth ions is small enough to be treated as a perturbation of the free ion spectra; this is also true for the actinide ions, at least in some crystals³⁻⁹. In a free ion, electric dipole transitions within a configuration are forbidden, but the odd parity part of the crystal potential will mix configurations of opposite parity so that "forced" electric dipole transitions can take place as well as the allowed magnetic dipole transitions. The strength of the forced electric dipole transition depends inversely upon the energy differences between mixing configurations^{10, 11}. In crystals containing triply ionized actinides total absorption begins at about 4000\AA , and it is assumed that this is due to the allowed $5f$ - $6d$ transitions. (Knowledge of the free ion spectra would be useful here). Since the analogous $4f$ - $5d$ transitions in rare earth crystals take place at about 2000 \AA^{12} , more intense spectra can be expected from this effect in actinide crystals than in rare earth crystals.

The ground configuration of U^{3+} is $5f^3$. Since nothing is known experimentally about the free ion spectrum of U^{3+} , we have made calculations on the $5f^3$ configuration to aid in the interpretation of crystal spectra.

II. FREE ION

The Hamiltonian for the free ion is

$$H_f = H_o + H_e + H_s$$

where H_o is the interaction of the 5f electrons with the core (constant for the configuration)

H_e is the electrostatic interaction between the three 5f electrons

H_s is the spin orbit interaction.

Higher order effects, including spin-spin and spin-other-orbit interactions will be neglected.

The electrostatic interaction is

$$H_e = \sum_{i>j} \frac{e^2}{r_{ij}} \quad i, j = 1, 2, 3$$

where electrons in closed shells are assumed to affect the energies of the 5f electrons only by a contribution to the central potential.

We can expand $\frac{1}{r_{ij}}$ in terms of the Legendre polynomials¹³

$$\frac{1}{r_{ij}} = \sum_{k=0}^{\infty} \frac{r_a^n}{r_b^n} P_n(\cos \omega)$$

where r_a is the smaller and r_b the larger of the distances of r_i and r_j from the nucleus, and ω is the angle between r_i and r_j . Then we can separate the radial and angular components and write

$$H_e = \sum_n f^n F_n \quad n = 2, 4, 6 \quad \text{for } f \text{ electrons} .$$

Matrix elements of f^n are essentially integrals of spherical harmonics over the angular wave function, and have been evaluated by Carlson¹⁴ for f^3 using Racah's method. The F_n are integrals of $\frac{r^n}{n+1}$ over the 5f radial wave functions (Slater integrals). If 5f hydrogenic wave functions are assumed, that is, in a Coulomb field, Judd¹⁵ has calculated

$$F_4/F_2 = 0.1422 \quad \text{and} \quad F_6/F_2 = 0.0161 .$$

The spin orbit interaction is

$$H_s = \sum_{i=1}^3 \xi(r_i) \vec{l}_i \cdot \vec{s}_i .$$

ξ , the integral of $\xi(r_i)$ over the radial wave function, is determined experimentally due to lack of knowledge of the wave function. The matrix elements of the angular part of H_s have been calculated for f^3 by Judd and Loudon¹⁶. In U^{3+} the spin orbit interaction is rather large, therefore we had to perform intermediate coupling calculations. Since J is a good quantum number, this involved diagonalizing matrices for each J value, $1/2$ to $17/2$. The electrostatic matrices, assuming 5f hydrogenic wave functions, and spin orbit matrices have been diagonalized simultaneously, by using a program developed

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-4-

by Wybourne*, for various values of $\chi = \zeta/F_2$ expressing energies in terms of F_2 and wave functions as linear combinations of Russell-Saunders states. Figure 1 shows the variation in energy levels of f^3 with χ , for $\chi = 7$ to 11. The levels are named by the Russell-Saunders states into which they go at $\zeta = 0$. For $F_2 = 200$, $\chi = 8$, (the order of magnitude appropriate for U^{3+})¹⁷, it is noted that the configuration extends $35,000 \text{ cm}^{-1}$. In comparison, the $Nd^{3+} 4f^3$ configuration extends $67,000 \text{ cm}^{-1}$. The 41 levels are each $(2J + 1)$ -fold degenerate.

The use of the 5f hydrogenic wave functions for U^{3+} is questionable. Lammermann and Conway⁸ feel that the Coulomb approximation is satisfactory for the interpretation of the $Pu^{3+}(5f^5)$ spectrum. Cohen has done a relativistic self-consistent calculation for the normal uranium ion, and Winocur has calculated the following set of Slater integrals from Cohen's eigenfunctions¹⁸

$$F_4/F_2 = 0.159 \quad F_6/F_2 = 0.0204.$$

The discrepancy between a similar calculation for PrIV and the experimental values indicates that these should be treated with reserve¹⁷.

McLaughlin⁹ determined F_2 , F_4 , and F_6 experimentally by a least squares fit to the spectrum of $UCl_4(5f^2)$ and found the ratios to be

* Private communication.

$$F_4/F_2 = 0.1468 \quad F_6/F_2 = 0.0219$$

We have calculated energy levels and wave functions of f^3 using these last ratios with $\chi = 8.0$, and the energy levels are compared with hydrogenic ones in Figure 2. F_2 has been chosen to put the $^4I_{11/2}$ level at 4500 cm^{-1} from the ground state where it has been observed^{19, 20}. It is apparent that the position of the $^4F_{3/2}$ level relative to the $^4I_{13/2}$ is depressed in the non-hydrogenic case, and above $10,000 \text{ cm}^{-1}$, where the energy levels become more dense, the grouping is much different in the two cases.

III. CRYSTAL FIELD

We are interested in crystals in which the splitting of the J manifold is small compared to the spin-orbit splitting, so in a first approximation the crystal field interaction can be treated as a perturbation of the free ion energy levels. However, since the $5f$ wave functions are more extensive than the $4f$ wave functions²², somewhat larger crystal field effects can be expected in the actinides than in the rare earths. Each J level of an ion with an odd number of electrons will split in a crystal field into $(2J + 1)/2$ components at the most due to Kramers degeneracy.

The Hamiltonian for the crystal field interaction, assuming a purely electrostatic field is²³

$$H_c = \sum_{kq} A_k^q \langle r^k \rangle V_k^q(\theta, \phi) \quad |q| \leq k, k = 2, 4, 6 \text{ for } f \text{ electrons.}$$

The number of terms in the expansion depends on the symmetry of the ion site in the crystal. The coefficients A_k^q depend on the lattice, and, although it is theoretically possible to calculate them if the positions and charge distributions of the ions in the crystal are known, results have not been satisfactory. Therefore, $A_k^q \langle r^k \rangle$ are customarily treated as experimentally determined parameters. The V_k^q are normalized associate spherical harmonics which transform in the same manner as the unit tensor operators U_k^q and are related to them by constant factors. We may use either set for calculations. Matrix elements of the crystal potential, for LS coupling then, can be obtained by using the relation¹⁵

$$\langle a LSJM | U_{\mathbf{q}}^k | a'L'S'J'M' \rangle = \delta(SS')(-1)^{J-M} \begin{pmatrix} J & kJ' \\ -M & q M' \end{pmatrix} \langle a LSJ || U^k || a'L'S'J' \rangle,$$

where the reduced matrix element is

$$\langle a LSJ || U^k || a'L'S'J' \rangle = (-1)^{S+k+L'+J} \left[(2J+1)(2J'+1) \right]^{1/2} \begin{Bmatrix} L & J & S \\ J' & L' & k \end{Bmatrix} \langle a LS || U^k || a'L'S \rangle.$$

3-j symbols $\begin{pmatrix} J & kJ' \\ -M & q M' \end{pmatrix}$ and 6-j symbols $\begin{Bmatrix} L & J & S \\ J' & L' & k \end{Bmatrix}$ are vector coupling coefficients and are available in tabular form²⁴. Judd has tabulated the double reduced matrix elements $\langle a LS || U^k || a'L'S \rangle$ for f³. If J mixing is neglected, the matrix elements may be more simply calculated from

$$\langle a LSJM | V_k^q | a'L'SJM' \rangle = \langle a LSJ || V_k || a'L'SJ \rangle f_k S_k^q(M),$$

where $S_k^q(M)$ are the Stevens coefficients²⁶ and the f_k , which depend only on J, are proportionality constants chosen to make the S_k^o integers.

U³⁺ states can be represented by linear combinations of Russell-Saunders states with coefficients depending on χ ; therefore the crystal field matrix elements will also depend on χ , and we have obtained them for $\Delta J = 0$ by the same transformation which diagonalized the 5f³ energy matrix.

Table I presents the results of calculations we have made on the 5f³ configuration using hydrogenic wave functions. For each J value for $\chi = 7.0$ to 11.0 , energies in units of F₂ are given in the first row. In the columns below each energy level are the coefficients

of the LS wave functions for that level. Reduced matrix elements in intermediate coupling are given in terms of $\langle aLSJ || V_k || bL'SJ \rangle$ $f_k \times 10^3$ in order that they may be used with the Stevens coefficients given in Table II^{26, 27}. The last row of each column gives the Landé g-value of the level in intermediate coupling.

As an example of the use of the tables, the splitting of a $^4F_{5/2}$ level in D_{3h} symmetry for $\chi = 8$ is $(-0.00937)S_2^0(M) + (-0.02391)S_4^0(M)$ or

$$(-0.00937) \times 5 \times A_2^0 + (-0.02391) \times 1 \times A_4^0 = -0.04685 A_2^0 - 0.02391 A_4^0, m=5/2$$
$$(-0.00937) \times (-1) \times A_2^0 - (0.02391) \times (-3) \times A_4^0 = 0.00937 A_2^0 + 0.07173 A_4^0, m=3/2$$
$$(-0.00937) \times (-4) \times A_2^0 - (0.02391) \times 2 A_4^0 = 0.03748 A_2^0 - 0.04782 A_4^0, m=1/2 .$$

In a crystal field J is only approximately a good quantum number, so that J levels will also be mixed. A complete J mixing calculation would involve diagonalizing three 60- and 61-dimensional matrices, and does not seem to be worthwhile until more is known about the wave functions. However, in order to get an idea of the magnitude involved, J mixing of the $^4I_{9/2}$ and $^4I_{11/2}$ states can be calculated by second order perturbation theory. (For higher levels which become more nearly degenerate this cannot be done).

We have calculated the splittings of the $^4I_{9/2}$ and $^4I_{11/2}$ states using 5f hydrogenic wave functions for $\chi = 8.0$ and the fictitious crystal field parameters

$$\begin{array}{ll} A_2^0 \langle r^2 \rangle = 170 & A_6^0 \langle r^6 \rangle = -100 \\ A_4^0 \langle r^4 \rangle = -80 & A_6^6 \langle r^6 \rangle = 1100 \end{array}$$

which are close to those found by Gruber⁴ for Am³⁺ in LaCl₃.

The effect of the ⁴I_{11/2} state on the ⁴I_{9/2} state 4500 cm⁻¹ below it is to depress the ground Stark level by 27 cm⁻¹ and to increase slightly the overall splitting. The calculated splittings of the ⁴I_{11/2} and ⁴I_{9/2} levels using the above parameters, with and without J mixing, are shown in Figure 3.

CONCLUSION

Experimentally, a complication occurs in uranium doped crystals in that uranium readily ionizes to U^{4+} and less easily to U^{3+} so that crystals nominally containing U^{3+} sometimes contain both ions, as was the case for $\text{CaF}_2:\text{U}^{3+}$.^{28, 29} The ground configuration of U^{4+} is $5f^2$. In Figure 4 we compare McLaughlin's energy level diagram for U^{4+} with our calculated one for $5f^3$ for reasonable values of F_2 and χ , and find that the energy levels are often very close, especially when we take into account Stark splitting, which could spread each level by several hundred cm^{-1} . However, a 1.88μ absorption line, described as characteristic of U^{3+} .^{28, 29} does not fit into the $5f^3$ energy level scheme. Either hydrogenic wave functions are decidedly in error or this 1.88μ line belongs to U^{4+} , where it could fit into the 3H_5 state.

It is difficult to see how these levels can be definitely assigned until the free ion spectra have been analyzed. Also it is quite desirable to know the position of the 6d configuration in order to estimate line strengths. Therefore, a program has been initiated to analyze the free ion spectra of ionized uranium. We hope to start with UIV (U^{3+}) and to go on to UIII and UV. This work will be done in cooperation with the Physics Department of The Johns Hopkins University.

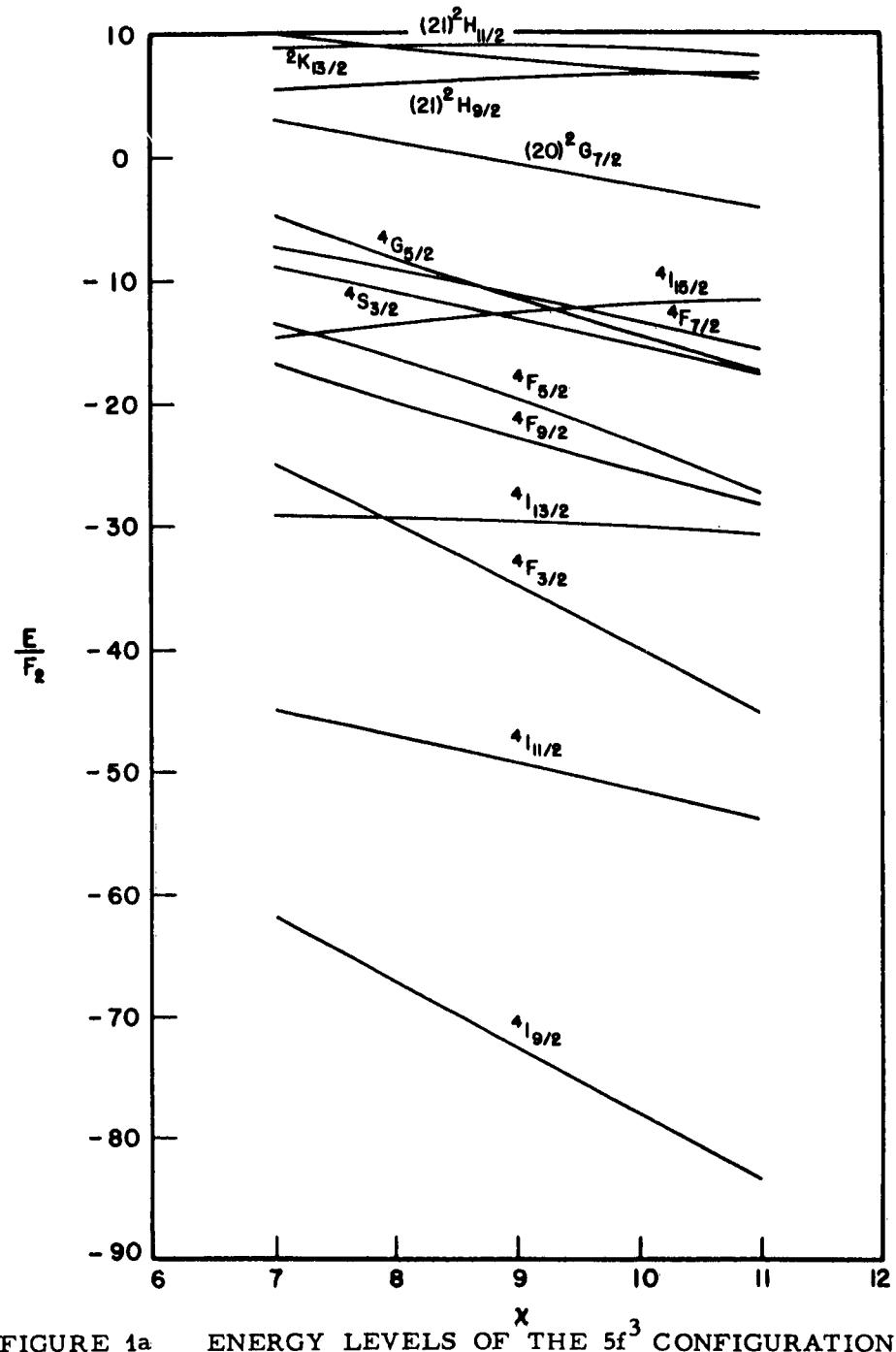


FIGURE 1a ENERGY LEVELS OF THE $5f^3$ CONFIGURATION.

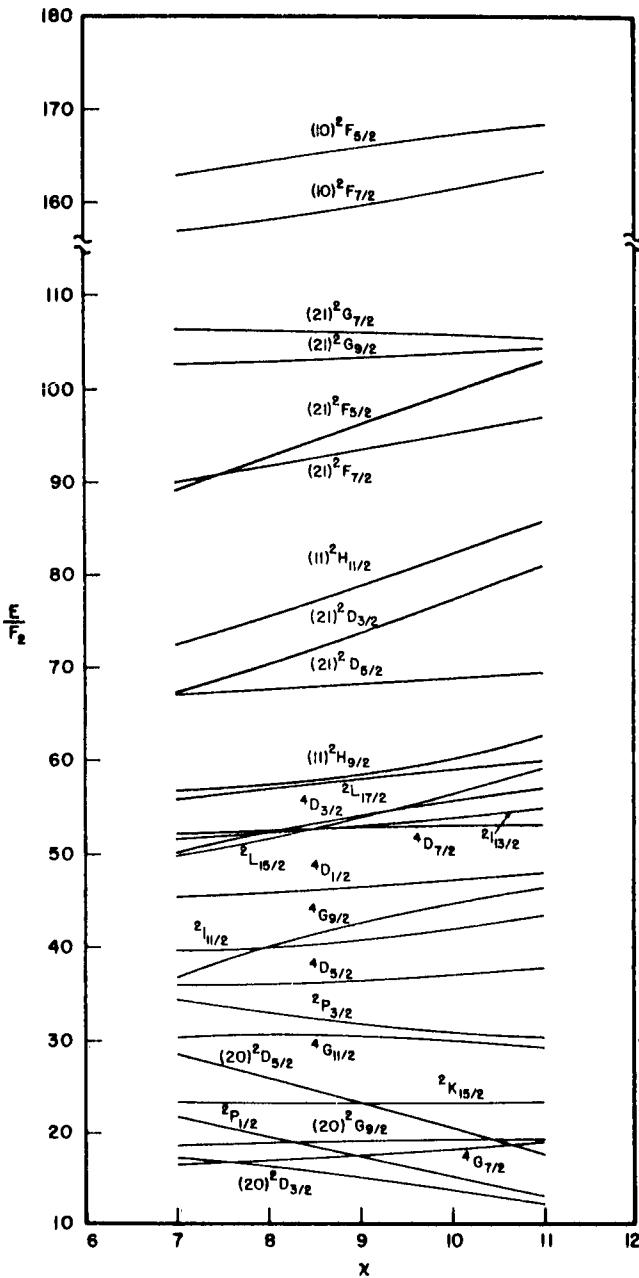


FIGURE 1b ENERGY LEVELS OF THE $5f^3$ CONFIGURATION.

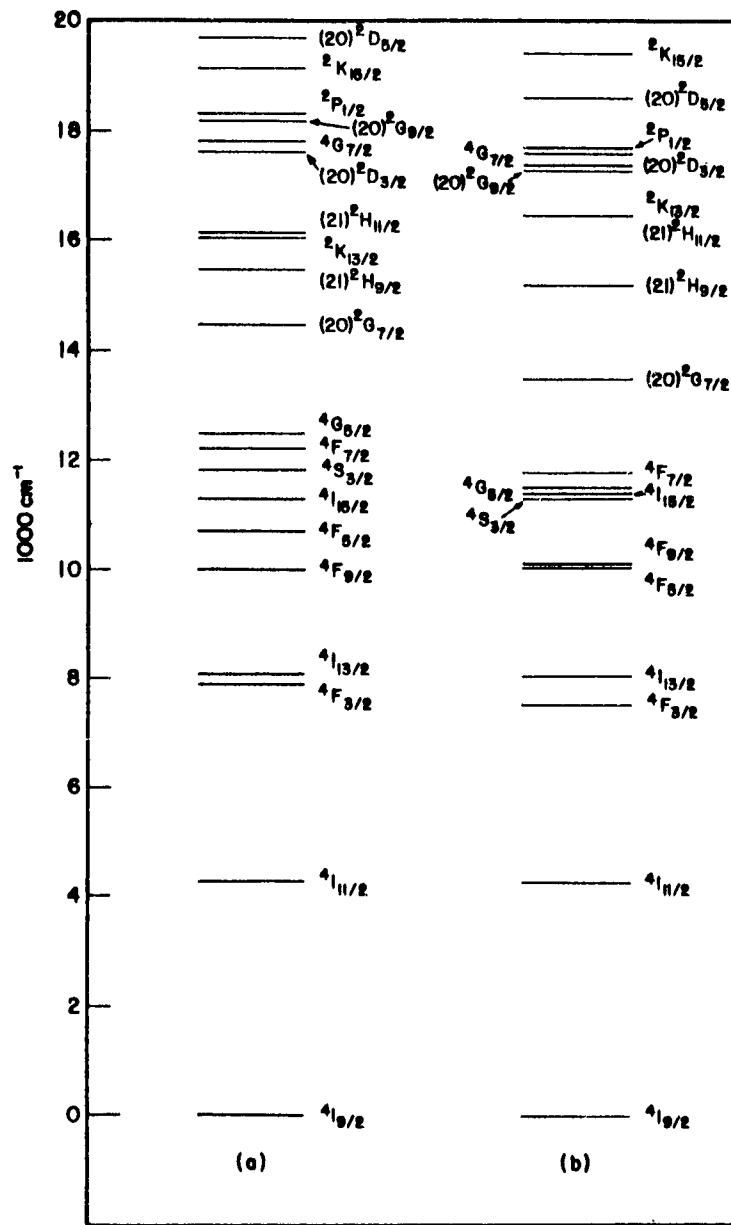


FIGURE 2 LOW-LYING ENERGY LEVELS OF THE $5f^3$ CONFIGURATION FOR $\chi = 8$.

(a) $F_2 = 211$ $F_4 = 30.004$ $F_6 = 3.3971$ (hydrogenic)
 (b) $F_2 = 213$ $F_4 = 31.098$ $F_6 = 4.6647$ (McLaughlin's ratios⁹)
 from U^{4+} .

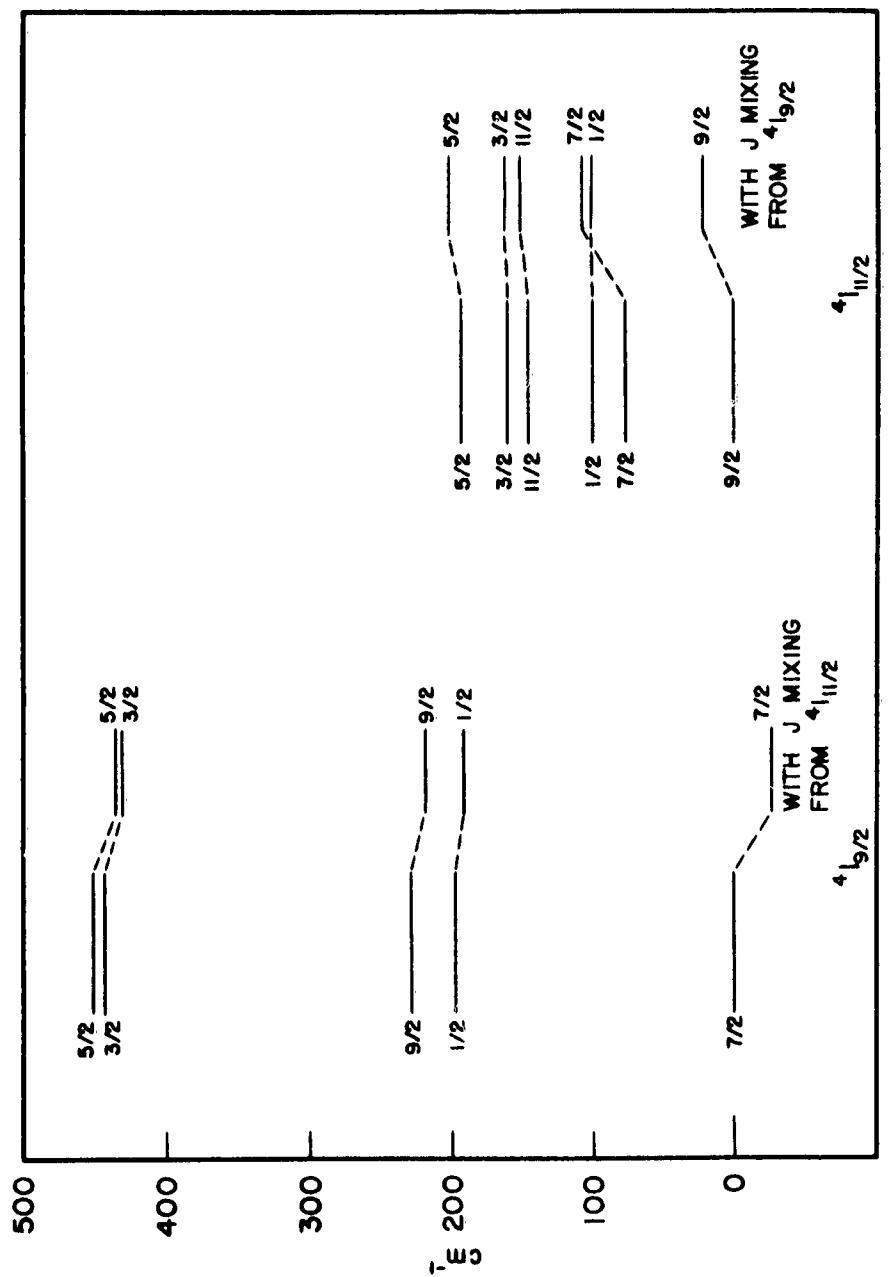


FIGURE 3 CRYSTAL FIELD SPLITTING IN A D_{3h} SYMMETRY SITE

$$\begin{array}{ll} A_2^0 \langle r^2 \rangle = 170 & A_6^0 \langle r^6 \rangle = -100 \\ A_4^0 \langle r^4 \rangle = -80 & A_6^0 \langle r^6 \rangle = 1100 \end{array}$$

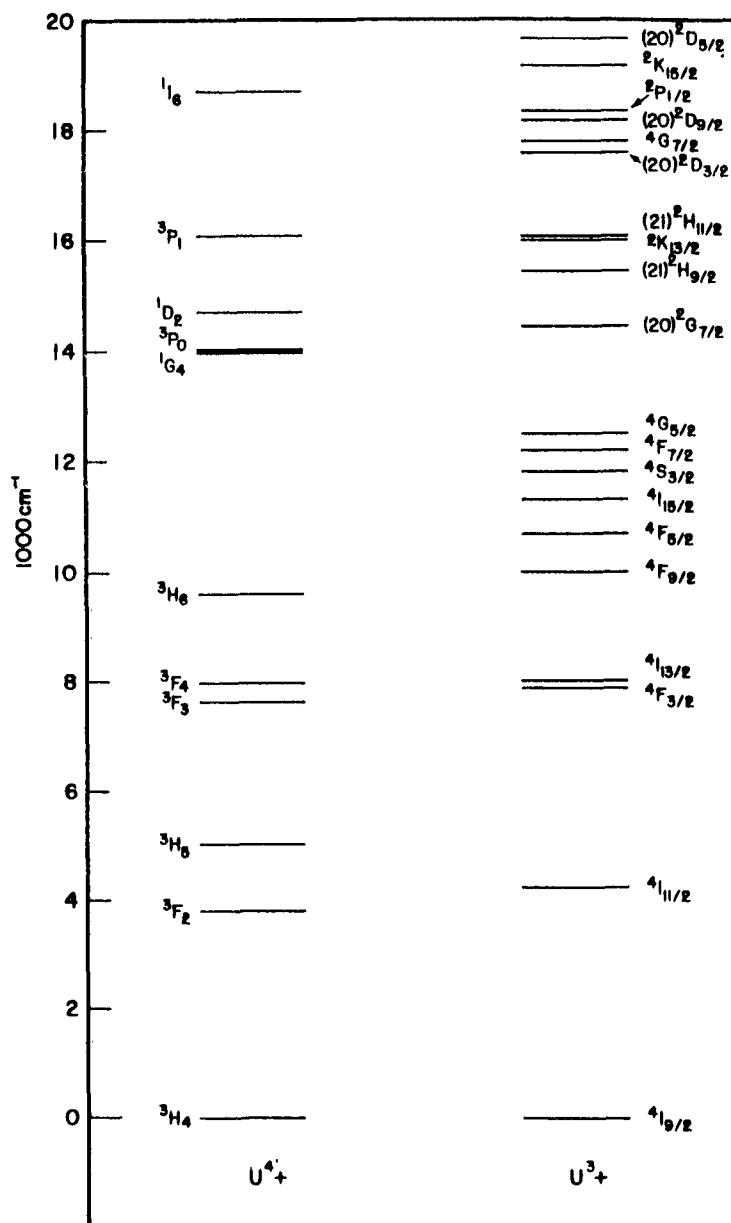


FIGURE 4 LOWER ENERGY LEVELS FOR U^{3+} AND U^{4+} .

$X = 7.0, J = 1/2$	$X = 9.0, J = 1/2$
EIGENVALUES	EIGENVALUES
21.714	45.335
EIGENVECTORS	EIGENVECTORS
2P 0.82131 -C.57645	2P 0.76853 -C.63581
4C 0.5705C C.82131	4C C.63982 C.76852
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING	REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING
F2V2 C.CCCC	F2V2 C.CCCC
F4V4 C.CCCC	F4V4 C.CCCC
F6V6 C.CCCC	F6V6 C.CCCC
G 0.4437C C.21697	G G.39376 C.227251
$X = 7.5, J = 1/2$	$X = 9.5, J = 1/2$
EIGENVALUES	EIGENVALUES
2C 713 45.586	16.461 46.835
EIGENVECTORS	EIGENVECTORS
2P 0.80665 -C.591C3	2P 0.75764 -C.65264
4C C.591C4 C.82C65	4C C.65263 C.75764
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING	REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING
F2V2 C.CCCC	F2V2 C.CCCC
F4V4 C.CCCC	F4V4 C.CCCC
F6V6 C.CCCC	F6V6 C.CCCC
G 0.4337S C.2328E	G G.38267 C.284CC
$X = 8.0, J = 1/2$	$X = 10.0, J = 1/2$
EIGENVALUES	EIGENVALUES
15.623 45.866	15.353 47.156
EIGENVECTORS	EIGENVECTORS
2P 0.79259 -C.60925	2P 0.74755 -C.66422
4C 0.6C924 C.79295	4C C.66422 C.74755
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING	REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING
F2V2 C.CCCC	F2V2 C.CCCC
F4V4 C.CCCC	F4V4 C.CCCC
F6V6 C.CCCC	F6V6 C.CCCC
G 0.41622 C.24745	G G.37255 C.29412
$X = 8.5, J = 1/2$	$X = 11.0, J = 1/2$
EIGENVALUES	EIGENVALUES
19.625 46.17C	13.696 47.933
EIGENVECTORS	EIGENVECTORS
2P 0.78C3C -C.62541	2P 0.72554 -C.68354
4C C.62542 C.78C3C	4C 0.68395 C.72554
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING	REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING
F2V2 C.CCCC	F2V2 C.CCCC
F4V4 C.CCCC	F4V4 C.CCCC
F6V6 C.CCCC	F6V6 C.CCCC
G 0.4C591 C.26G7E	G G.35881 C.3118E

TABLE I. WAVE FUNCTIONS, ENERGIES, AND REDUCED MATRIX ELEMENTS OF $5f^3$.

$x = 7.5^*, j = 3/2$		$x = 3.5^*, j = 3/2$	
EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS
4S -C.15247 C.38643 0.45168 -0.13778 -C.29225 -0.08990	4S -C.16866 C.79618 0.48111 0.21976 -C.20515 -0.12654		
4P -C.22134 C.43417 0.45158 -0.27697 C.59253 -0.32271	4P -C.26628 C.465CC 0.36634 -0.14082 -C.3245 -0.3630		
12C1C 0.42229 -C.C8175 0.51121 0.39595 C.53972 0.38598	(2C1C 0.46329 -C.C7631 0.33201 0.39419 C.47368 -0.5936		
(21)2C 0.14716 C.C0665 -0.25120 0.44605 -0.43382 0.49162	(21)2C 0.46329 -C.C7631 0.33201 0.39419 C.47368 -0.5936		
4C -G.C6836 C.C7025 0.34335 0.73992 C.23990 0.48850	4C -G.C8292 C.C828C 0.43329 0.66404 C.38575 -0.54599		
4F 0.28476 C.J1132 -0.36139 -0.68724 -0.26527 -0.03953	4F 0.8AC601 C.3654 0.38664 -0.11620 -C.21423 -0.07056		
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING	REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING		
F2v2 11.2228 76.7151 34.7121 -57.4063 -101.5398 176.2628	F2v2 95.655 99.1154 36.6652 -38.4211 -25.5405 281.5520		
F4v4 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	F4v4 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000		
F6v6 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	F6v6 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000		
G C.56854 1.7072E 1.15173 1.Ca088 1.05403 0.97638	G 0.61336 1.62442 1.09077 1.03651 1.00165		
$x = 7.5^*, j = 3/2$		$x = 9.0^*, j = 3/2$	
EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS
4S -2.293 -5.952 1.63871 33.655 51.314 63.693	4S -2.17173 C.78332 0.48300 0.24384 -C.20483 -0.13754		
4P -0.23555 C.82345 0.46667 0.16369 -0.20407 -0.10254	(20)2C 0.71434 -C.C7383 0.33245 -0.37574 C.30290 0.5386		
(20)2C 0.44213 -C.C9664 0.44612 -0.29354 -0.29874 0.57002 0.38444	(21)2C 0.81115 -C.C346 0.25758 -0.62925 -C.53413 0.38283		
(21)2C -0.15229 -C.CC24 -0.29168 0.49222 -0.44297 0.56227	4C -C.09165 0.6251 0.6251 0.33613 C.61041 -0.44207		
4C -0.07551 C.C7511 -0.37311 0.71503 0.32753 -0.47887	4F 0.193344 C.18553 -0.38834 -0.13455 -0.21591		
4F 0.33132 C.3335C 0.37736 -0.03903 -0.20906 -0.05015	REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING		
F2v2 101.771C 25.9424 25.2438 -52.5226 -142.C223 215.5876	F2v2 95.9103 1.C5.LC2 -7.9753 -29.8449 -231.0416 307.8472		
F4v4 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	F4v4 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000		
F6v6 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	F6v6 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000		
G C.5944C 1.678CC 1.1500C 1.0825G 1.04869 0.98175	G 0.6264C 1.60224 1.09476 1.03395 1.01649 1.00165		
$x = 6.0^*, j = 3/2$		$x = 9.5^*, j = 3/2$	
EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS
-2.747 -11.047 16.383 32.917 52.313 70.213	-2.7359 -14.427 14.643 31.227 54.943 75.262		
4S -C.1631C C.3C54C 0.47576 0.19116 -0.20497 -0.11482	4S -0.1782 C.77231 0.49181 0.27808 C.20418 -0.14776		
2P -C.2489C C.453C 0.39772 -0.32109 0.54724 0.41144	2P -0.2806 C.47824 -0.30316 -0.37314 C.49477 -0.47793		
12C1C 0.45441 -C.C7833 0.46035 0.37166 C.49559 0.43779	(20)2C 0.4335C -C.C7833 0.31289 0.43562 -0.45537		
(21)2C -0.16431 -C.CG128 0.36035 0.36035 C.48221 0.48559	(21)2C -0.18894 -C.C0455 0.33201 0.44857 C.55212 0.55884		
4C -G.C8267 C.C8162 0.4C328 0.69014 C.35815 -0.46756	4C -G.C1191 C.6925 0.40203 0.60737 -0.42229		
4F -0.21924 C.25134 -0.38107 -0.03986 -C.2120 -0.06057	4F C.38154 C.35953 -0.38007 -0.15362 0.21721 -0.08874		
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING	REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING		
F2v2 1C3.5677 92.7436 14.8233 -46.0711 -175.3461 250.3035	F2v2 92.4406 11G.6751 -19.7803 -20.7323 -252.5767 329.735		
F4v4 C.CCCC 0.C000 0.0000 0.0000 0.0000 0.0000 0.0000	F4v4 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000		
F6v6 C.CCCC 0.C000 0.0000 0.0000 0.0000 0.0000 0.0000	F6v6 C.CCCC 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000		
G 0.59936 1.65G34 1.16233 1.0858C 1.04346 0.99205	G 0.63852 1.57776 1.163349 1.10516 1.02985 1.G1655		

TABLE I CONTINUED.

$x = 1C, C, j = 3/2$		$x = 7C, C, j = 5/2$			
EIGENVALUES		EIGENVALUES			
4S -0.17125	C.761554	0.30654	C.2C3332	-0.15720	
2P -C.28945	C.42435	-0.27218	-C.62444	0.-49468	
(20) 2C C.49111	-C.62775	0.34293	0.53537	C.-13.69	
(21) 2C C.-18634	-C.-C0634	-C.-4C516	-C.-62724	0.-53659	
4C -0.-1C723	C.-1C723	0.-1605	0.-45155	-0.-41660	
4F C.-77021	C.41455	-0.32640	-0.17222	C.21380	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING		REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING			
F2V2 85.1934	115.8674	-311.4121	111.4755	-270.5437	
F4V4 C.CCCC	0.CCCC	0.0000	0.CCCC	0.0000	
F6V6 C.CCCC	0.CCCC	0.0000	0.CCCC	0.0000	
G C.6976	1.55652	1.16051	1.11405	1.02584	
$x = 11C, j = 3/2$		$x = 7.5, C, j = 5/2$			
EIGENVALUES		EIGENVALUES			
4S -C.13133	C.74224	-0.46487	0.3594C	C.2C110	-0.17335
2P -C.93562	C.-C616	0.1334	-C.-42767	-C.-52163	0.34293
(20) 2C 0.5C362	-C.6816	-0.24945	0.3824	-C.38016	0.53213
(21) 2C C.10835	C.44613	0.56015	0.2115	-C.-43378	-0.39324
4F C.74973	C.43555	0.17981	-0.20758	C.21993	-0.-11037
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING		REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING			
F2V2 82.3071	125.2223	-53.C1C0	6.1665-297.6540	375.9855	
F4V4 C.CCCC	0.CCCC	0.CCCC	0.CCCC	0.CCCC	
F6V6 C.CCCC	0.CCCC	0.0000	0.CCCC	0.0000	
G 0.66795	1.31957	1.15195	1.13193	1.02028	
$x = 8C, C, j = 5/2$		$x = 8.5C, C, j = 5/2$			
EIGENVALUES		EIGENVALUES			
4S -16.373	-8.18C	25.984	35.932		
EIGENVECTORS		EIGENVECTORS			
(20) 2C 0.30295	C.C0165	0.48887	0.78111		
(21) 2C 0.C375	-C.C0165	0.51405	-0.16408		
4C C.C203C	-C.C0155	0.5425	-0.51894		
(10) 2C F.0.14365	C.17254	0.17254	0.17118		
(21) 2C F.-0.1414C	C.16241	-0.16163	0.24206		
4F C.87683	C.23641	0.15395	0.4180		
4G C.-0.3117C	C.28681	0.17981	-0.0819		
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING		REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING			
F2V2 -5.372C	51.9C7	-27.7188	51.1632		
F4V4 -23.9142	334.9C3E-108.3774	-56.0625	-81.4693-135.5577		
F6V6 C.0CCC	0.0CCC	0.0000	0.0000		
G 0.69324	C.6933C	1.2239	1.08164		

TABLE I CONTINUED.

EIGENVALUES		EIGENVALUES	
-16.373	-8.18C	25.984	35.932
EIGENVECTORS		EIGENVECTORS	
(20) 2C 0.30295	C.C0165	0.48887	0.78111
(21) 2C 0.C375	-C.C0165	0.51405	-0.16408
4C C.C203C	-C.C0155	0.5425	-0.51894
(10) 2C F.0.14365	C.17254	0.17254	0.17118
(21) 2C F.-0.1414C	C.16241	-0.16163	0.24206
4F C.87683	C.23641	0.15395	0.4180
4G C.-0.3117C	C.28681	0.17981	-0.0819
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING		REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING	
F2V2 -5.372C	51.9C7	-27.7188	51.1632
F4V4 -23.9142	334.9C3E-108.3774	-56.0625	-81.4693-135.5577
F6V6 C.0CCC	0.0CCC	0.0000	0.0000
G 0.69324	C.6933C	1.2239	1.08164

$X = 8.5, \zeta = 5/2$	EIGENVECTORS	-17.932	24.688	36.088	67.999	94.308	174.906	
EIGENVECTORS	-17.932	-9.895	24.688	36.088	67.999	94.308	174.906	
(12)1C0	C-0.552	C-1.143	0.43345	0.81147	-0.17037	-0.10890	-0.03420	
(12)1C0	C-0.552	C-0.9013	0.55446	-0.16112	-0.34002	-0.73957	-0.04239	
(12)1C0	C-0.4778	-C-0.6480	0.64814	-0.48114	-0.55715	-0.28337	-0.05603	
4D	0.64800	-0.48114	0.55715	-0.28337	-0.42952	-0.18777	-0.75981	
(11)1C0F	-0.16255	C-1.15967	-0.18059	0.60603	0.42952	0.41877	-0.18385	
F4	0.44784	C-0.42921	-0.16774	0.08323	0.39125	-0.66778	0.20912	
4F	0.44784	C-0.21162	0.19337	-0.06464	-0.21640	0.10544	-0.05594	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING								
F212	-15.3394	34.3266	-35.3109	58.157	0.025114	-41.66118	-0.05453	
F44	-35.3395	34.3266	-124.6787	-16.7031	-78.4345	135.811	221.2666	
F64	C-COCC	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
G	C-0.57539	C-0.7814	1.21192	1.22058	1.05148	-0.88559	0.85690	
$X = 9.0, \zeta = 5/2$	EIGENVALUES	-15.594	-11.56C	23.331	36.321	68.296	96.055	175.563
EIGENVECTORS	-15.594	-11.56C	23.331	36.321	68.296	96.055	175.563	
(12)01C0	C-0.50756	C-1.365	0.33143	C-0.1797	-0.11434	-0.03635		
(12)1C0	C-0.55445	-C-0.9277	0.54378	-0.09952	-0.32006	0.74495	-0.04696	
4C	0.55445	C-0.6511C	0.6511C	-0.45322	0.55118	-0.29394	0.09960	
(11)1C0F	-0.19120	C-0.19121	0.18446	-0.43430	0.41563	-0.73561	0.11015	
(21)1C0F	-0.17582	C-0.17582	0.15444	-0.17149	0.08359	-0.53632	-0.47165	
4F	C-0.17137	C-0.4662C	0.17394	-0.28254	0.03841	0.15388	-0.00647	
4G	-0.19137	C-0.83855	C-0.21557	-0.05764	-0.22759	-0.13441	-0.05236	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING								
F212	-21.8395	65.06C	88.819	61.067	-0.8931	115.188	-188.2089	
F44	-42.915C	15C.115C	-135.895C	-22.463	-77.310	-135.541	217.8319	
F64	C-COCC	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
G	0.55448	C-0.70442	1.21014	1.212551	1.04488	1.09458	0.86000	
$X = 9.5, \zeta = 5/2$	EIGENVALUES	-21.365	-13.168	21.939	36.607	68.600	97.816	176.233
EIGENVECTORS	-21.365	-13.168	21.939	36.607	68.600	97.816	176.233	
(12)1C0	C-0.20569	C-1.64597	0.35345	0.84238	C-0.17938	-0.11936	0.03854	
(12)1C0	C-0.64866	C-0.9491	0.56466	-0.07745	-0.30114	0.76923	-0.05176	
4C	0.64866	C-0.44938	C-0.7154	-0.63338	-0.22952	0.55265	-0.30649	
(11)1C0F	-0.19253	C-0.19253	0.16202	-0.18698	0.55040	-0.43377	0.414351	
(21)1C0F	-0.17551	C-0.17551	0.14711	-0.17354	0.06773	0.56380	0.35872	
4F	C-0.17144	C-0.50359	0.15193	-0.17515	0.29187	-0.03754	-0.11215	
4G	-0.17144	C-0.83054	C-0.23116	-0.053379	-0.23466	-0.13502	-0.022646	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING								
F212	-25.444	7C.5033	-C-0.447	66.5558	1.5784	-1.0287	-188.3359	
F44	5C.6662	-14.7898	87.794	-0.7485	134.7696	214.2479		
F64	C-COCC	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
G	C-0.53281	C-73251	1.2C747	1.21155	1.04279	1.09875	0.88645	

TABLE I CONTINUED.

$\lambda = 7.5, \beta^2 = 7/2$		$\lambda = 9, C_{ij} = 7/2$	
EIGENVALUES		EIGENVALUES	
-8.251	2.124	16.839	52.532
0.1373	-0.02829	0.17132	90.846
0.5646	-0.12073	0.19433	90.409
0.1411	-0.07614	0.11764	167.499
0.8423	0.14462	0.26837	0.11836
0.2112	-0.05937	0.09837	-0.03924
0.7647	-0.02940	0.0316	-0.12526
0.4570	-0.02940	0.0316	0.14274
0.2012	-0.45862	0.18151	0.60683
0.2112	0.57151	0.06111	-0.14274
0.3868	-0.6994	0.0094	-0.73367
0.2235	0.26262	-0.06457	-0.13217
F2V2	0.10115	-0.44974	-0.04255
F4V4	31.4531	-29.3395	-37.3421
F6V6	36.4603	29.3395	41.3260
F8V8	51.4531	-32.2525	48.3260
F10V10	55.8824	55.6151	54.7710
F12V12	55.9856	1.1087	-47.3998
F14V14	55.9856	1.14202	91.91258
F16V16	55.9856	1.14202	1.31319
F18V18	55.9856	1.14202	1.91541
F20V20	55.9856	1.14202	98.1541
F22V22	55.9856	1.14202	101.2695
F24V24	55.9856	1.14202	101.2695
F26V26	55.9856	1.14202	101.2695
F28V28	55.9856	1.14202	101.2695
F30V30	55.9856	1.14202	101.2695
F32V32	55.9856	1.14202	101.2695
F34V34	55.9856	1.14202	101.2695
F36V36	55.9856	1.14202	101.2695
F38V38	55.9856	1.14202	101.2695
F40V40	55.9856	1.14202	101.2695
F42V42	55.9856	1.14202	101.2695
F44V44	55.9856	1.14202	101.2695
F46V46	55.9856	1.14202	101.2695
F48V48	55.9856	1.14202	101.2695
F50V50	55.9856	1.14202	101.2695
F52V52	55.9856	1.14202	101.2695
F54V54	55.9856	1.14202	101.2695
F56V56	55.9856	1.14202	101.2695
F58V58	55.9856	1.14202	101.2695
F60V60	55.9856	1.14202	101.2695
F62V62	55.9856	1.14202	101.2695
F64V64	55.9856	1.14202	101.2695
F66V66	55.9856	1.14202	101.2695
F68V68	55.9856	1.14202	101.2695
F70V70	55.9856	1.14202	101.2695
F72V72	55.9856	1.14202	101.2695
F74V74	55.9856	1.14202	101.2695
F76V76	55.9856	1.14202	101.2695
F78V78	55.9856	1.14202	101.2695
F80V80	55.9856	1.14202	101.2695
F82V82	55.9856	1.14202	101.2695
F84V84	55.9856	1.14202	101.2695
F86V86	55.9856	1.14202	101.2695
F88V88	55.9856	1.14202	101.2695
F90V90	55.9856	1.14202	101.2695
F92V92	55.9856	1.14202	101.2695
F94V94	55.9856	1.14202	101.2695
F96V96	55.9856	1.14202	101.2695
F98V98	55.9856	1.14202	101.2695
F100V100	55.9856	1.14202	101.2695
F102V102	55.9856	1.14202	101.2695
F104V104	55.9856	1.14202	101.2695
F106V106	55.9856	1.14202	101.2695
F108V108	55.9856	1.14202	101.2695
F110V110	55.9856	1.14202	101.2695
F112V112	55.9856	1.14202	101.2695
F114V114	55.9856	1.14202	101.2695
F116V116	55.9856	1.14202	101.2695
F118V118	55.9856	1.14202	101.2695
F120V120	55.9856	1.14202	101.2695
F122V122	55.9856	1.14202	101.2695
F124V124	55.9856	1.14202	101.2695
F126V126	55.9856	1.14202	101.2695
F128V128	55.9856	1.14202	101.2695
F130V130	55.9856	1.14202	101.2695
F132V132	55.9856	1.14202	101.2695
F134V134	55.9856	1.14202	101.2695
F136V136	55.9856	1.14202	101.2695
F138V138	55.9856	1.14202	101.2695
F140V140	55.9856	1.14202	101.2695
F142V142	55.9856	1.14202	101.2695
F144V144	55.9856	1.14202	101.2695
F146V146	55.9856	1.14202	101.2695
F148V148	55.9856	1.14202	101.2695
F150V150	55.9856	1.14202	101.2695
F152V152	55.9856	1.14202	101.2695
F154V154	55.9856	1.14202	101.2695
F156V156	55.9856	1.14202	101.2695
F158V158	55.9856	1.14202	101.2695
F160V160	55.9856	1.14202	101.2695
F162V162	55.9856	1.14202	101.2695
F164V164	55.9856	1.14202	101.2695
F166V166	55.9856	1.14202	101.2695
F168V168	55.9856	1.14202	101.2695
F170V170	55.9856	1.14202	101.2695
F172V172	55.9856	1.14202	101.2695
F174V174	55.9856	1.14202	101.2695
F176V176	55.9856	1.14202	101.2695
F178V178	55.9856	1.14202	101.2695
F180V180	55.9856	1.14202	101.2695
F182V182	55.9856	1.14202	101.2695
F184V184	55.9856	1.14202	101.2695
F186V186	55.9856	1.14202	101.2695
F188V188	55.9856	1.14202	101.2695
F190V190	55.9856	1.14202	101.2695
F192V192	55.9856	1.14202	101.2695
F194V194	55.9856	1.14202	101.2695
F196V196	55.9856	1.14202	101.2695
F198V198	55.9856	1.14202	101.2695
F200V200	55.9856	1.14202	101.2695
F202V202	55.9856	1.14202	101.2695
F204V204	55.9856	1.14202	101.2695
F206V206	55.9856	1.14202	101.2695
F208V208	55.9856	1.14202	101.2695
F210V210	55.9856	1.14202	101.2695
F212V212	55.9856	1.14202	101.2695
F214V214	55.9856	1.14202	101.2695
F216V216	55.9856	1.14202	101.2695
F218V218	55.9856	1.14202	101.2695
F220V220	55.9856	1.14202	101.2695
F222V222	55.9856	1.14202	101.2695
F224V224	55.9856	1.14202	101.2695
F226V226	55.9856	1.14202	101.2695
F228V228	55.9856	1.14202	101.2695
F230V230	55.9856	1.14202	101.2695
F232V232	55.9856	1.14202	101.2695
F234V234	55.9856	1.14202	101.2695
F236V236	55.9856	1.14202	101.2695
F238V238	55.9856	1.14202	101.2695
F240V240	55.9856	1.14202	101.2695
F242V242	55.9856	1.14202	101.2695
F244V244	55.9856	1.14202	101.2695
F246V246	55.9856	1.14202	101.2695
F248V248	55.9856	1.14202	101.2695
F250V250	55.9856	1.14202	101.2695
F252V252	55.9856	1.14202	101.2695
F254V254	55.9856	1.14202	101.2695
F256V256	55.9856	1.14202	101.2695
F258V258	55.9856	1.14202	101.2695
F260V260	55.9856	1.14202	101.2695
F262V262	55.9856	1.14202	101.2695
F264V264	55.9856	1.14202	101.2695
F266V266	55.9856	1.14202	101.2695
F268V268	55.9856	1.14202	101.2695
F270V270	55.9856	1.14202	101.2695
F272V272	55.9856	1.14202	101.2695
F274V274	55.9856	1.14202	101.2695
F276V276	55.9856	1.14202	101.2695
F278V278	55.9856	1.14202	101.2695
F280V280	55.9856	1.14202	101.2695
F282V282	55.9856	1.14202	101.2695
F284V284	55.9856	1.14202	101.2695
F286V286	55.9856	1.14202	101.2695
F288V288	55.9856	1.14202	101.2695
F290V290	55.9856	1.14202	101.2695
F292V292	55.9856	1.14202	101.2695
F294V294	55.9856	1.14202	101.2695
F296V296	55.9856	1.14202	101.2695
F298V298	55.9856	1.14202	101.2695
F300V300	55.9856	1.14202	101.2695
F302V302	55.9856	1.14202	101.2695
F304V304	55.9856	1.14202	101.2695
F306V306	55.9856	1.14202	101.2695
F308V308	55.9856	1.14202	101.2695
F310V310	55.9856	1.14202	101.2695
F312V312	55.9856	1.14202	101.2695
F314V314	55.9856	1.14202	101.2695
F316V316	55.9856	1.14202	101.2695
F318V318	55.9856	1.14202	101.2695
F320V320	55.9856	1.14202	101.2695
F322V322	55.9856	1.14202	101.2695
F324V324	55.9856	1.14202	101.2695
F326V326	55.9856	1.14202	101.2695
F328V328	55.9856	1.14202	101.2695
F330V330	55.9856	1.14202	101.2695
F332V332	55.9856	1.14202	101.2695
F334V334	55.9856	1.14202	101.2695
F336V336	55.9856	1.14202	101.2695
F338V338	55.9856	1.14202	101.2695
F340V340	55.9856	1.14202	101.2695
F342V342	55.9856	1.14202	101.2695
F344V344	55.9856	1.14202	101.2695
F346V346	55.9856	1.14202	101.2695
F348V348	55.9856	1.14202	101.2695
F350V350	55.9856	1.14202	101.2695
F352V352	55.9856	1.14202	101.2695
F354V354	55.9856	1.14202	101.2695
F356V356	55.9856	1.14202	101.2695
F358V358	55.9856	1.14202	101.2695
F360V360	55.9856	1.14202	101.2695
F362V362	55.9856	1.14202	101.2695
F364V364	55.9856	1.14202	101.2695
F366V366	55.9856	1.14202	101.2695
F368V368	55.9856	1.14202	101.2695
F370V370	55.9856	1.14202	101.2695
F372V372	55.9856	1.14202	101.2695
F374V374	55.9856	1.14202	101.2695
F376V376	55.9856	1.14202	101.2695
F378V378	55.9856	1.14202	101.2695
F380V380	55.9856	1.14202	101.2695
F382V382	55.9856	1.14202	101.2695
F384V384	55.9856	1.14202	101.2695
F386V386	55.9856	1.14202	101.2695
F388V388	55.9856	1.14202	101.2695
F390V390	55.9856	1.14202	101.2695
F392V392	55.9856	1.14202	101.2695
F394V394	55.9856	1.14202	101.2695
F396V396	55.9856	1.14202	101.2695
F398V398	55.9856	1.14202	101.2695
F400V400	55.9856	1.14202	101.2695
F402V402	55.9856	1.14202	101.2695
F404V404	55.9856	1.14202	101.2695
F406V406	55.9856	1.14202	101.2695
F408V408	55.9856	1.14202	101.2695
F410V410	55.9856	1.14202	101.2695
F412V412	55.9856	1.14202	101.2695
F414V414	55.9856	1.14202	101.2695
F416V416	55.9856	1.14202	101.2695
F418V418	55.9856	1.14202	101.2695
F420V420	55.9856	1.14202	101.2695
F422V422	55.9856	1.14202	101.2695
F424V424	55.9856	1.14202	101.2695
F426V426	55.9856	1.14202	101.2695
F428V428	55.9856	1.14202	101.2695
F430V430	55.9856	1.14202	101.2695
F432V432	55.9856	1.14202	101.2695

TABLE I CONTINUED.

TABLE I CONTINUED.

x = 10.C, j = 9/2										
EIGENVALUES					EIGENVECTORS					
EIGENVECTORS					EIGENVECTORS					
-75.878	-21.232	6.241	19.01C	41.451	57.779	103.181	-77.935	-25.516	6.768	
4F	-0.C224	-C.3363C	0.79145	-0.C152	0.48698	0.13730	C.3191C	-C.33616	0.77446	
(2C)G	-0.C8043	-C.4353C	0.4239	0.54525	0.12275	0.45455	(2C)126	-0.C9345	C.43835	
(21)2G	-0.C746	-C.37415	0.63005	0.5986	0.24429	0.38907	(21)26	-0.87649	C.28C76	
(21)2G	-0.C746	-C.37415	0.63005	0.5986	0.24429	0.38907	(21)26	-0.87649	C.28C76	
4G	0.04440	-C.25257	0.16741	0.12637	-0.19864	0.71231	4S	-C.4551	-C.-6115	
(11)2h	0.12046	-C.22115	0.08386	0.24986	0.24986	0.24986	(11)2h	-C.1237	-C.-0.0552	
(21)2h	-C.36723	C.57018	0.16333	0.49751	0.25357	0.49751	(21)2h	-0.59816	C.3325C	
4I	C.511C	C.34914	0.16333	0.49751	0.25357	0.49751	(21)2h	-0.59816	C.3325C	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING										
F212	-26.2704	37.3665	18.4934	0.2187	13.8102	-25.5362	-65.0668	F212	-26.1627	
F44	-16.4865	2.7752	-18.934	11.1594	13.6331	-1.7556	3.3228	F44	-17.2671	
F646	-15.4221	55.7412	-39.4136	9.9460	2.4481	19.8055	-78.8337	F646	-12E.5747	
G	0.76042	1.0171C	1.18971	1.12338	1.10453	0.97407	1.09790	G	0.76725	
x = 11.C, j = 9/2										
EIGENVALUES					EIGENVECTORS					
-75.543	-22.671	6.440	19.097	42.717	58.374	103.387	-63.358	-26.321	6.980	
4F	C.C2922	-C.33622	0.78261	0.C0356	0.-48562	0.16755	0.6434	0.C3545	-C.3362C	
(20)15	-0.C8357	C.43555	-0.23704	0.04994	0.49395	0.16568	0.64427	(20)126	-C.-1C15	
(21)15	0.67911	-C.21702	0.09776	0.09595	-C.25610	0.45560	0.70095	(21)26	C.9522	
4G	0.47476	-C.-55451	-0.18395	0.905C	0.02518	0.27772	-0.05239	(11)26	-0.5218	
(11)3h	C.-12334	-C.-21706	0.-0.057	-0.30431	-0.35317	0.80594	0.6287	(11)2h	-C.13259	
(21)12h	-C.-37845	C.-56004	0.49772	0.25366	-0.45234	0.12318	0.08977	(21)12h	-0.41522	
4I	C.S0325	C.-26C21	0.17190	0.19848	-0.C7444	0.-0.05133	0.02294	4I	C.88661	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING										
F212	-27.5459	37.5517	15.9035	1.957C	5.715C	-61.9283	F212	-24.8579	3.4272	
F44	-16.C65	2.6276	-19.1461	11.5072	13.-8951	-18.1847	F44	-16.5154	2.0131	
F646	-135.734C	S2.31CC	-41.603	59.3157	13.7014	6.9479	-79.6991	F646	-121.858	79.2552
G	0.76275	1.01748	1.18817	1.12466	1.09488	0.98819	1.09666	G	0.77149	1.C1556
x = 9.C, j = 9/2										
EIGENVALUES					EIGENVECTORS					
-75.878	-22.225	-28.CCS	6.617	19.-178	43.829	59.137	103.-618			
4F	0.C3C13	-C.33617	0.78C64	C.02496	C.48097	0.19987	0.00984			
(20)15	-C.C9321	C.43617	-0.24420	0.05617	C.31517	0.19159	0.64733			
(21)15	-C.88318	-C.21751	0.05010	0.10122	-C.31867	-0.49039	0.69316			
4G	0.05C13	-C.-55817	-0.24427	0.99546	-0.31057	0.28935	-0.05103			
(11)2h	0.12557	-C.-13117	-0.05610	-0.31836	-0.46082	0.76888	0.27587			
(21)1h	-C.38874	C.35C4	0.49714	0.26686	-C.-46040	0.08540	0.19207			
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING										
F212	-26.284C	37.3152	13.1466	3.8343	-3.0459	-10.1036	-62.7853			
F44	-17.6645	2.4758	-19.3191	11.826C	13.-9350	-2.2164	54.8649			
F646	-132.1015	38.9312	-43.6423	63.5842	25.3226	-6.2967	-80.5628			
G	0.76523	1.C1718	1.18678	1.12079	1.08384	1.CC033	1.09527			

TABLE I CONTINUED.

$X = 7.0, J = 11/2$										
EIGENVALUES					EIGENVECTORS					
-44.734					C.44293					
4G	0.C2769	-C.44293	0.66939	-0.18852	C.27431	4G	C.C3441	-C.4844C	0.47385	
(11)2h	0.-C1758	-C.25566	-0.61274	-0.24711	C.70189	(11)2h	0.C8221	-C.18675	0.-0.7172C	
(21)2h	-0.18254	C.32143	0.22916	-0.16946	C.55891	(21)2h	-0.2C317	C.79813	0.-0.22724	
21	-0.C3CC6	-C.17713	0.27720	0.81905	C.46902	21	-C.C3163	C.23864	0.-0.4500C	
4I	C.57549	C.17682	0.07783	0.C2598	C.03935	4I	C.S7446	C.19112	0.1C688	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING										
F2V2	-2.8749	C.6147	-2.C331	-7.1947	-3.9488	F2V2	-3.8168	C.1795	-4.4371	
F4V4	-1C.6334	3.-8471	14.-5838	28.-2027	1C.5498	F4V4	-1C.4335	7.0517	-3.-8146	
F6V6	-2C.4488	-26.-5C34	-13.-3387	-11.-6099	62.-7741	F6V6	-15.-9618	-3C.3862	25.-2643	
G	C.57613	1.11724	1.16618	1.C2162	1.06748	G	0.57141	1.111942	12.-7931	
$X = 8.0, J = 11/2$										
EIGENVALUES					EIGENVECTORS					
-45.949					C.45817					
4G	C.C998	-C.-45817	0.62845	-0.55659	C.29058	4G	C.C654	-C.49532	0.40003	
(11)2h	0.C77C7	-C.-23432	-0.65612	-0.18466	C.68904	(11)2h	C.C525	-C.16055	0.-73556	
(21)2h	-0.C1511	C.-81352	0.22705	-0.18052	C.46603	(21)2h	-0.2C512	C.78554	0.-0.1057	
21	-0.C1332	C.-19652	0.33964	0.78945	C.47093	21	-C.C41C	C.-2611C	0.-2.574	
4I	0.S7778	C.18448	C.C8747	0.02114	C.-0.0249	4I	C.S7286	C.1929C	0.-69G5C	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING										
F2V2	-3.855C	C.-8633	-6.-3023	-3.-9067	F2V2	-3.7584	-C.C115	-5.C176	0.-0.0551	
F4V4	-1C.5973	4.-842C	13.-4450	27.-4958	11.-3133	F4V4	-1C.-35C1	8.-2627	11.-1525	C.05161
F6V6	-2C.-2821	-27.-5522	-8.-9124	-14.-170C	62.-0.0880	F6V6	-15.-8085	-31.-538C	1.-5033	-18.-9085
G	0.57057	1.-11831	1.-14239	1.C4258	1.C6880	G	0.57182	1.-11937	1.-0.07944	1.C9825
$X = 8.5, J = 11/2$										
EIGENVALUES					EIGENVECTORS					
-46.971					C.472CC					
4G	C.C3222	-C.-472CC	C.55144	-0.61508	C.30621	4G	C.C3861	-C.5047C	0.-33211	
(11)2h	0.-77997	-C.-11335	-C.-63114	-0.-11644	C.67694	(11)2h	0.C8773	-C.13295	0.-0.71525	
(21)2h	-C.19684	C.80622	0.22589	-0.-19093	C.47304	(21)2h	-C.21474	C.76C34	0.-6.4099	
21	-C.C3250	-C.217C4	0.357C	0.75589	C.47192	21	-C.C3571	C.-28456	0.-2.0988	
4I	0.S761C	C.18626	0.69721	0.C165C	C.04559	4I	0.S713C	C.19414	0.-6.63352	
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING										
F2V2	-3.-8357	C.3463	-3.-6986	-5.-3818	F2V2	-2.78C6	-C.2254	-5.-4267	0.-3.7144	
F4V4	-10.-5125	5.91C3	12.-5487	26.-3903	12.-C25	F4V4	-1C.2718	5.5255	10.-4.588	14.-1854
F6V6	-2.-1196	-29.-1512	-4.-7940	-16.-3877	61.-3140	F6V6	-15.-66CC	-32.-5858	3.-3309	-19.-2370
G	0.57C95	1.-119C5	1.-11853	1.063377	1.07032	G	0.57221	1.11885	1.06595	1.07557

TABLE I CONTINUED

$x = 10 \cdot C, J = 11/2$ EIGENVALUES $\begin{array}{llll} -51.525 & 8.871 & 29.819 & 41.986 \\ & & & 82.128 \end{array}$ EIGENVECTORS $\begin{array}{llll} 4G & G \cdot C4C63 & -C \cdot S1248 & -0 \cdot 27047 \\ (11)2r & G \cdot C9CC4 & -C \cdot 10414 & 0 \cdot 75647 \\ (21)2r & -C \cdot 200C4 & C \cdot 77C46 & -0 \cdot 25237 \end{array}$ $\begin{array}{llll} 21 & -C \cdot 33667 & C \cdot 32845 & -0 \cdot 52195 \\ 41 & 0 \cdot 56975 & C \cdot 19425 & -0 \cdot 11590 \\ F2V2 & -3 \cdot 7633 & -C \cdot 7334 & -5 \cdot 6798 \end{array}$ $\begin{array}{llll} F4V4 & -1C \cdot 1956 & 10 \cdot 8554 & 9 \cdot 6943 \\ F6V6 & -15 \cdot 1561 & -33 \cdot 508C & 5 \cdot 2038 \end{array}$ $\begin{array}{llll} G & 0 \cdot 9726C & 1 \cdot 11794 & 1 \cdot 05616 \\ & & & 1 \cdot 11849 \end{array}$ $1 \cdot 07746$	$x = 7 \cdot C, J = 13/2$ EIGENVALUES $\begin{array}{llll} -25. C22 & 1C \cdot CCS & 51.564 & \\ & & & \end{array}$ EIGENVECTORS $\begin{array}{llll} 2I & -C \cdot C7516 & -C \cdot 1938J & \\ 6I & C \cdot S7215 & 0 \cdot 21466 & 0 \cdot 03247 \\ 2K & 0 \cdot 20265 & C \cdot 9572C & 0 \cdot 2C535 \end{array}$ $\begin{array}{llll} \text{REDUCED MATRIX ELEMENTS IN INTERMEDIATE CCUPLING} & & & \\ F2V2 & -2C \cdot 3037 & -56 \cdot 2375 & -37 \cdot 3045 \\ F4V4 & -2 \cdot 3937 & -5 \cdot 0065 & 4 \cdot 3037 \\ F6V6 & -3 \cdot 6541 & 1 \cdot 6542 & 1 \cdot 1C76 \\ G & 1 \cdot 10228 & C \cdot 9467E & 1 \cdot 07090 \end{array}$
$x = 11 \cdot C, J = 11/2$ EIGENVALUES $\begin{array}{llll} -53. 841 & 3. 375 & 29. 268 & 43. 337 \\ & & & 85. 636 \end{array}$ EIGENVECTORS $\begin{array}{llll} 4G & 0 \cdot C4449 & -C \cdot S23C5 & -0 \cdot 16381 \\ (11)2r & 0 \cdot C943C & -C \cdot C4. 25 & 0 \cdot 76439 \\ (21)2r & -C \cdot 228SC & C \cdot 74847 & -C \cdot 28359 \end{array}$ $\begin{array}{llll} 21 & -0 \cdot C3847 & -C \cdot 35693 & -0 \cdot 53241 \\ 41 & 0 \cdot 56687 & C \cdot 192C4 & -0 \cdot 15265 \\ F2V2 & -3 \cdot 73C2 & -1 \cdot 0. 355 & -5 \cdot 3216 \end{array}$ $\begin{array}{llll} F4V4 & -1C \cdot 493 & 13 \cdot 3891 & 7 \cdot 9357 \\ F6V6 & -15 \cdot 2419 & -34 \cdot 9C7 & 7 \cdot C007 \end{array}$ $\begin{array}{llll} G & 0 \cdot 97335 & 1 \cdot 11463 & 1 \cdot 04516 \\ & & & 1 \cdot 12822 \end{array}$ $1 \cdot C8129$	$x = 7.5, J = 13/2$ EIGENVALUES $\begin{array}{llll} -25. 1C2 & 9 \cdot 456 & 51. 946 & \\ & & & \end{array}$ EIGENVECTORS $\begin{array}{llll} 4I & C \cdot S7152 & -C \cdot 23455 & 0 \cdot 03374 \\ 2K & 0 \cdot 22223 & C \cdot 55122 & 0 \cdot 214C3 \end{array}$ $\begin{array}{llll} \text{REDUCED MATRIX ELEMENTS IN INTERMEDIATE CCUPLING} & & & \\ F2V2 & -2C \cdot 6558 & -55 \cdot 8811 & -37 \cdot 3092 \\ F4V4 & -2 \cdot 3925 & -4 \cdot 9215 & 4 \cdot 2186 \\ F6V6 & -3 \cdot 521C & 1 \cdot 6958 & 1 \cdot C428 \\ G & 1 \cdot C9887 & C \cdot 9486S & 1 \cdot 07038 \end{array}$
$x = 3 \cdot C, J = 13/2$ EIGENVALUES $\begin{array}{llll} -25. 216 & 8 \cdot 531 & 52. 336 & \\ & & & \end{array}$ EIGENVECTORS $\begin{array}{llll} 2I & -0 \cdot C8962 & -C \cdot 2063C & C \cdot 27438 \\ 4I & C \cdot S6635 & -C \cdot 25487 & 0 \cdot 03493 \\ 2K & C \cdot 24115 & C \cdot 54471 & 0 \cdot 22221 \end{array}$ $\begin{array}{llll} \text{REDUCED MATRIX ELEMENTS IN INTERMEDIATE CCUPLING} & & & \\ F2V2 & -21 \cdot 047C & -55 \cdot 482C & -37 \cdot 2165 \\ F4V4 & -2 \cdot 3931 & -4 \cdot 84C7 & 4 \cdot 137C \\ F6V6 & -3 \cdot 45CC & 1 \cdot 6863 & C \cdot 9819 \\ G & 1 \cdot C9731 & C \cdot 95C77 & 1 \cdot 06987 \end{array}$	

TABLE I CONTINUED

```

X= 9.C. J= 13/2          X= 7.C. J= 15/2
EIGENVALUES      EIGENVALUES
-25.55C          -14.71C
-25.55C          -23.31E
7.957           49.94E
53.134           56.053

EIGENVECTORS     EIGENVECTORS
-21.05432 -C-2159E  -0.97076
-0.54432 -C-2945C  0.03108
2K 0.27583 C.5363C  0.23718
REduced MATRIX ELEMENTS IN INTERMEDIATE CCUPLING
F2Y2 -21.9481 -54.56C4 -37.3315
F4V4 -2.3514 -4.6892 3.9839
F6V6 -3.288C 1.6352 0.8704
G 1.C937C C.95536 1.06689

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```

X= 9.5, J= 13/2          X= 7.5, J= 15/2
EIGENVALUES           EIGENVALUES
-25.773              -14.057
EIGENVECTORS          EIGENVECTORS
21 -0.11262 -C.21582   0.96902
41 0.54745 -C.31764   0.03006
2K 0.29544 C.92238 C.24405
REDUCE MATRIX ELEMENTS IN INTERMEDIATE CCUPLING
F2V2 -22.570 +0.086 -37.350
F4V4 -3.389 -4.6185  3.9194
F6V6 -3.1958 1.5541  0.8194
G 1.C5167 C.55186 1.0842

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```

X= 1C. C, J= 13/2
EIGENVALUES
-2C.034   7.129   53.955
EIGENVECTRS
-2C.12052 -C.22307  0.96733
-2C.33987 0.03893
0.54033 -C.33987
0.31911 0.51141  0.25054
0.25054
REFUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING
F2Y2 -23.CC2S -53.4186 -37.3666
F4V4 -2.3875 -4.5531  3.8432
F6V6 -2.0567  1.5432  0.7712
G  1.C0945  C.5659C  1.06756
X= 8.0, J= 15/2
EIGENVALUES
-13.49C  23.282   51.755
EIGENVECTRS
-13.49C  23.282   51.755
EIGENVECTRS
4I  0.51395 -C.3726C -C.1661B  0.000C
2K  0.358C  C.6744I  C.6652C  0.000C
2L  -0.105C -C.6152C  0.7752C  0.000C
2L  0.CCCC  C.CCCC  0.CCCC  1.000C
REDUCED MATRIX ELEMENTS IN INTERMEDIATE CCU
F2Y2 -1C.21C1 -26.525C -29.8915 -19.6076
F4V4 -2.54C8 -C.88C7  -3.7292 -3.5651
F6V6 -24.4355 -7.6127  1.4970  1.6876
G  1.17653  1.C662C  0.96449  1.0590C

```

$\alpha = 11.0, \beta = 13/2$	EIGENVALUES	EIGENVECTORS	REDUCED MATRIX ELEMENTS IN INTERMEDIATE STATES
	-2C-6.672	6.427	54.795
	-2C-6.672	6.427	0.96408
	2I - C 13.651	-C -22.786	0.06067
	4I 0.52359	-C 38.123	0.22522
	2K 0.25827	C 89.556	0.22522
	F2V2 -24.1558	-51.25456	-37.955
	F4V4 -3.3821	-6.4266	3.7139
	F6V6 -2.87852	1.4144	0.66244
	6 J -1.87454	C 56.613	1.06708

TABLE I (CONTINUED)

MR 705

X= 8.5, J= 15/2		X= 10.0, J= 15/2		X= 11.5, J= 15/2	
EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS
-12.982	23.246	52.791	57.553	-11.97C	23.16S
41 0.50075 -C.393C7 -0.18478 0.0000C	41 0.85543 C.45916 -0.23962 0.0000C	41 0.85543 C.45916 -0.23962 0.0000C	41 0.85543 C.45916 -0.23962 0.0000C	41 0.85543 C.45916 -0.23962 0.0000C	41 0.85543 C.45916 -0.23962 0.0000C
2K 0.41560 C.65635 0.42965 0.0000C	2K 0.46270 -C.58324 0.66764 0.0000C	2K 0.46270 -C.58324 0.66764 0.0000C	2K 0.46270 -C.58324 0.66764 0.0000C	2K 0.46270 -C.58324 0.66764 0.0000C	2K 0.46270 -C.58324 0.66764 0.0000C
15 2L -0.12622 -C.64356 0.75456 0.0000C	15 2L -0.1629C C.68434 0.71074 0.0000C	15 2L -0.1629C C.68434 0.71074 0.0000C	15 2L -0.1629C C.68434 0.71074 0.0000C	15 2L -0.1629C C.68434 0.71074 0.0000C	15 2L -0.1629C C.68434 0.71074 0.0000C
17 2L C.CCCC0 C.CCCC 0.0000C 1.0000C	17 2L 0.CCCCC C.CCCC 0.0000C 1.0000C				
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING					
F2V2 -1C.6269 -2C.7555 -29.2478 -19.6078	F2V2 -12.0616 -27.4826 -19.6078	F2V2 -12.0616 -27.4826 -19.6078	F2V2 -12.0616 -27.4826 -19.6078	F2V2 -12.0616 -27.4826 -19.6078	F2V2 -12.0616 -27.4826 -19.6078
F4V4 -2C.6254 -C.752C -3.8392 -3.5651	F4V4 -2C.6532 -4.C736 -3.5651	F4V4 -2C.6532 -4.C736 -3.5651	F4V4 -2C.6532 -4.C736 -3.5651	F4V4 -2C.6532 -4.C736 -3.5651	F4V4 -2C.6532 -4.C736 -3.5651
F6V6 -23.8641 -7.7638 14.0767 1.6876	F6V6 -22.0022 -8.0816 12.5327 1.6876				
G 1.17285 1.C3522 0.95977 1.0590C	G 1.16005 1.C3323 1.01456 1.0590C				
X= 9.0, J= 15/2		X= 11.5, J= 15/2		X= 11.5, J= 15/2	
EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS
-12.564	23.212	53.908	58.053	-11.699	23.156
41 0.88656 -C.41554 -0.2033C 0.0000C	41 0.82125 C.50C2E -0.27438 0.0000C	41 0.82125 C.50C2E -0.27438 0.0000C	41 0.82125 C.50C2E -0.27438 0.0000C	41 0.82125 C.50C2E -0.27438 0.0000C	41 0.82125 C.50C2E -0.27438 0.0000C
2K 0.43962 C.619C 0.44995 0.0000C	2K 0.52488 -C.47375 0.7C715 0.0000C	2K 0.52488 -C.47375 0.7C715 0.0000C	2K 0.52488 -C.47375 0.7C715 0.0000C	2K 0.52488 -C.47375 0.7C715 0.0000C	2K 0.52488 -C.47375 0.7C715 0.0000C
15 2L -0.1444C6 -C.65652 C.73225 0.0000C	15 2L -0.22376 C.72476 0.65166 0.0000C	15 2L -0.22376 C.72476 0.65166 0.0000C	15 2L -0.22376 C.72476 0.65166 0.0000C	15 2L -0.22376 C.72476 0.65166 0.0000C	15 2L -0.22376 C.72476 0.65166 0.0000C
17 2L 0.CCCCC C.CCCCC 0.0000C 1.0000C					
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING					
F2V2 -1L.C797 -2C.92C2 -28.63C7 -19.6078	F2V2 -13.2C79 -26.9734 -26.4493 -19.6078				
F4V4 -2C.6C25 -0.7255 -3.9321 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651
F6V6 -23.2654 -7.2872 13.6013 1.6876	F6V6 -2C.6336 -8.2385 11.3708 1.6876				
G 1.1688C 1.C34C5 1.0C489 1.0590C	G 1.15031 1.G3412 1.02341 1.0590C				
X= 9.5, J= 15/2		X= 11.5, J= 15/2		X= 11.5, J= 15/2	
EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS	EIGENVALUES	EIGENVECTORS
-12.227	23.185	55.098	58.553	-11.699	23.156
41 0.87143 C.43761 -0.22162 0.0000C	41 0.82125 C.50C2E -0.27438 0.0000C				
2K 0.46270 -C.58324 0.66764 0.0000C	2K 0.52488 -C.47375 0.7C715 0.0000C				
15 2L -0.1629C C.68434 0.71074 0.0000C	15 2L 0.CCCCC C.CCCCC 0.0000C 1.0000C				
17 2L C.CCCC0 C.CCCC 0.0000C 1.0000C	17 2L 0.CCCCC C.CCCCC 0.0000C 1.0000C	17 2L 0.CCCCC C.CCCCC 0.0000C 1.0000C	17 2L 0.CCCCC C.CCCCC 0.0000C 1.0000C	17 2L 0.CCCCC C.CCCCC 0.0000C 1.0000C	17 2L 0.CCCCC C.CCCCC 0.0000C 1.0000C
REDUCED MATRIX ELEMENTS IN INTERMEDIATE COUPLING					
F2V2 -1L.C567C -27.0216 -28.C421 -19.6078	F2V2 -13.2C79 -26.9734 -26.4493 -19.6078	F2V2 -13.2C79 -26.9734 -26.4493 -19.6078	F2V2 -13.2C79 -26.9734 -26.4493 -19.6078	F2V2 -13.2C79 -26.9734 -26.4493 -19.6078	F2V2 -13.2C79 -26.9734 -26.4493 -19.6078
F4V4 -2C.5658 -G.16 -C.097 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651	F4V4 -2C.6571 -4.C668 -3.5651
F6V6 -22.6432 -7.991C 13.C831 1.6876	F6V6 -2C.6336 -8.2385 11.3708 1.6876				
G 1.16455 1.C3343 1.0C983 1.0590C	G 1.15031 1.G3412 1.02341 1.0590C				

TABLE I CONTINUED

J	K	d ²	1000 f	M											
				1/2	3/2	5/2	7/2	9/2	11/2	13/2	15/2	17/2	19/2	21/2	
3/2	2	4.5	223.606 798	-1	1										
5/2	2	4,3,5,7	48.795 005	-4	-1	5									
	4	36,7	62.994 079	2	-3	1									
7/2	2	4,2,3,5,7	34.503 279	-5	-3	1	7								
	4	36,2,7,11	13.430 383	9	-3	-13	7								
	6	4,2,3,11,13	17.069 718	-5	9	-5	1								
9/2	2	4,3,5,11	38.924 947	-4	-3	-1	2	6							
	4	36,5,11,13	6.232 980	18	3	-17	-22	18							
	6	4,3,5,11,13	10.795 838	-8	6	10	-11	3							
11/2	2	4,3,5,7,11,13	4.080 444	-25	-29	-17	1	25		55					
	4	36,2,7,11,13	3.724 918	28	12	-13	-33	-27	53						
	6	4,2,3,11,13,17	4.140 015	-20	4	25	11	-31	11						
13/2	2	4,2,5,7,13	16.574 839	-8	-7	-5	-2	2	7	13					
	4	36,2,7,11,13,17	0.903 425	108	63	-13	-92	-132	-77	143					
	6	4,5,7,11,13,17,19	0.393 248	-200	-25	185	227	-11	-319	143					
15/2	2	16,3,5,7,17	5.917 263	-21	-19	-15	-9	-1	9	21	35				
	4	144,7,13,17,19	0.486 068	189	129	23	-101	-201	-221	-91	273				
	6	16,3,5,13,17,19	0.996 142	-75	-25	45	87	59	-39	-117	65				
17/2	2	36,2,5,17,19	2.932 564	-40	-37	-31	-22	-10	5	23	44	68			
	4	36,2,11,17,19	1.977 134	44	33	13	-12	-36	-51	-47	-12	68			
	6	36,11,13,17,19,23	0.161 702	-440	-209	145	439	481	169	-377	-650	442			
19/2	2	4,3,5,7,11,19	3.375 221	-33	-31	-27	-21	-13	-3	9	23	39	57		
	4	36,2,5,7,11,17,19,23	0.069 848	1188	948	503	-77	-687	-1187	-1402	1122	-102	1938		
	6	100,2,3,11,13,17,19,23	0.039 609	-1716	-988	195	1353	1931	1497	6	-1870	-2346	1938		
21/2	2	4,5,7,11,23	5.313 439	-20	-19	-17	-14	-10	1	8	16	25			
	4	36,5,7,11,13,19,23	0.112 695	702	585	365	70	-258	-563	-775	-810	-570	57	1197	
	6	4,3,5,11,13,17,19,23	0.125 254	-520	-338	-30	303	537	558	306	-170	-646	646		

(a) S_K⁰

J	7/2, -5/2	9/2, -3/2	11/2, -1/2	13/2, 1/2	15/2, 3/2	17/2, 5/2	19/2, 7/2	21/2, 9/2
7/2	0.755 929							
9/2	1.000 000	0.654 654						
11/2	2.309 401	1.825 782	1.023 533					
13/2	22.135 944	18.956 090	13.403 080	6.904 105				
15/2	8.090 398	7.236 272	5.693 469	3.765 875	1.837 559			
17/2	46.669 049	42.878 566	35.874 782	26.739 484	16.911 535	7.946 248		
19/2	179.885 676	158.267 644	146.458 185	117.166 548	84.005 184	51.497 573	23.531 134	
21/2	54.048 920	51.202 214	45.796 652	36.384 024	29.732 138	20.752 510	12.401 997	5.546 342

(b) S₆⁶

TABLE II. STEVENS COEFFICIENTS

ADDITIONAL TABLES OF S_K^q MAY BE FOUND IN REFERENCE 2.

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